

documents and visual observations did not reveal conditions which are considered to constitute a hazard to human life and property.

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SECURITY CLASSIFICATION OF THIS PAGE (From Date Entered)

The upstream face and portions of the downstream slope of the dam are covered with large trees, requiring clearing under the supervision of a professional engineer. The spillway apron slab was found to be undermined and the concrete is deteriorated, requiring repairs.

The spillway capacity was evaluated according to the recommended procedure and was found to pass 70 percent of the Probable Maximum Flood (PMF) without overtopping the dam. Because the spillway capacity is less than the recommended spillway design flood of full PMF, the spillway capacity is rated to be inadequate.



GENESEE RIVER BASIN

DANSVILLE RESERVOIR DAM

STEUBEN COUNTY, NEW YORK INVENTORY NO. N.Y. 431



PREPARED FOR

NEW YORK DISTRICT CORPS OF ENGINEERS
AUGUST 1981

APPROVED FOR PUBLIC RELEACT;

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PREFACE

This report is prepared under the guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM DANSVILLE RESERVOIR DAM N.Y. 431 DEC I.D. NO. 42-999 GENESEE RIVER BASIN STEUBEN COUNTY, NEW YORK

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^{*}Not included due to lack of pertinent data.

PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM

Name of Dam:

Dansville Reservoir Dam

N.Y. 431

State Located:

New York

County Located:

Steuben

Stream:

Little Mill Creek (a tributary of

Mill Creek)

Date of Inspection:

June 26, 1981 and July 15, 1981

ASSESSMENT

Based on the evaluation of the existing conditions, Dansville Reservoir Dam is considered to be in fair condition. The examination of documents and visual observations did not reveal conditions which are considered to constitute a hazard to human life and property.

The upstream face and portions of the downstream slope of the dam are covered with large trees, requiring clearing under the supervision of a professional engineer. The spillway apron slab was found to be undermined and the concrete is deteriorated, requiring repairs.

The spillway capacity was evaluated according to the recommended procedure and was found to pass 70 percent of the Probable Maximum Flood (PMF) without overtopping the dam. Because the spillway capacity is less than the recommended spillway design flood of full PMF, the spillway capacity is rated to be inadequate.

The following recommendations should be implemented within 12 months from notification to the owner:

- The trees on the upstream and downstream faces of the dam should be removed under the supervision of a professional engineer. Trees and brush on the earth embankments flanking the concrete overflow section of the spillway should also be cleared.
- 2. The spillway structures should be repaired.
- 3. An emergency action plan should be developed, including a formal warning system to alert the downstream residents in the event of emergencies.
- 4. The dam and appurtenant structures should be inspected regularly and necessary maintenance should be performed.

Assessment - Dansville Reservoir Dam

Market Colors
THONWEAT THE
PROFESSIONAL TO Lawrence D. Andersen Engineer Na. 174584
Lawrence D. Andersen
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MINING WAYLVANILLE
Medition 11

Lawre ce D. Andersen, P.E.

Vice resident

D'App lonia Consulting Engineers, Inc.

Pittsturgh, Pennsylvania

Approved by:

W. M. Smith, Jr.

New York District Engineer

Date:





PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM
DANSVILLE RESERVOIR DAM
N.Y. 431
DEC I.D. NO. 42-999
GENESEE RIVER BASIN
STEUBEN COUNTY, NEW YORK

SECTION 1: PROJECT INFORMATION

1.1 GENERAL

a. Authority

The Phase I Inspection reported herein was authorized by the Department of the Army, New York District, Corps of Engineers, to fulfill the requirements of the National Dam Inspection Act, Public Law 92-367.

b. Purpose of Inspection

The inspection was to evaluate the existing conditions of the dam to identify deficiencies and hazardous conditions, to determine if they constitute hazards to life and property, and to recommend remedial measures where necessary.

1.2 DESCRIPTION OF PROJECT

a. Dam and Appurtenances

The Dansville Reservoir Dam consists of an earth embankment having a maximum height of approximately 54 feet above its downstream toe and a crest width of 16 feet. The embankment gradually merges into the abutments and the limits of the embankment are not well defined. The length of the dam appears to be about 470 feet. The upstream and downstream faces are covered with brush and large trees. The upstream face has a measured slope of 2.2 horizontal to 1 vertical, and the downstream face has a measured slope of 2 horizontal to 1 vertical.

The spillway of the dam consists of a concrete ogee overflow section located approximately 2,400 feet northwest of the dam near the upstream end of the reservoir. This spillway is located across a natural saddle point and discharges into an adjacent watershed to the west of the reservoir. The ogee overflow section is approximately 100 feet long and 5.5 feet deep. The concrete overflow sections are flanked by earth embankments on each side. The flanking earth embankments are approximately eight feet high adjacent to the spillway structure and gradually merge into the abutments. The flanking embankments were designed to have a 2.5 horizontal to 1 vertical upstream slope, a 2 horizontal to 1 vertical downstream slope, a crest width of 5 feet and a total crest length of approximately 150 feet. The tops of the earth embankments are approximately 2.5 feet below the dam crest level.

The dam is equipped with two cast iron drainpipes (12 inches and 18 inches in diameter) which extend from the upstream embankment toe to the downstream toe. Flow through these pipes is controlled by a manually operated valve located in a valve chamber on the dam crest near the center of the dam.

b. Location

The dam is located on Little Mill Creek, approximately 2.6 miles upstream from its confluence with Mill Creek, east of Dansville in Wayland Township, Stuben County, New York. Plate 1 illustrates the location of the dam and spillway.

c. Size Classification

The dam is classified as an intermediate dam based on its 54-foot height and 954 acre-feet maximum storage capacity.

d. Hazard Classification

The dam is in the high hazard category. Little Mill Creek flows through an uninhabited valley for approximately 2.5 miles. Approximately 1.2 miles downstream from the dam, Little Mill Creek flows through a culvert, under a high (approximately 80-foot) abandoned railroad embankment. The culvert is about 350 feet long and approximately 16 feet wide by 14 feet high. Dansville is located approximately three miles downstream from the dam, a New York State Route 63 bridge is located 2.6 miles downstream, and six residences about 2.7 miles downstream from the dam are considered to be within the potential floodplain of Mill Creek in the event of a dam failure.

It is estimated that failure of the dam under maximum pool level would cause loss of more than a few lives and appreciable property damage in this area.

e. Ownership

The dam is owned by the Village of Dansville, 14 Clara Barton Street, Village of Dansville, New York 14437, 716-335-5270. Attention: Mr. Keith Petti, Superintendent.

f. Purpose of Dam

The dam is a water supply reservoir.

g. Design and Construction History

The date of construction of the dam is unknown. The dam was designed in 1933 by Frank H. Macy, Consulting Engineer, from Rochester, New York.

h. Normal Operating Procedure

The reservoir is normally maintained below the crest level of the spillway by periodically opening the low level outlet pipe. The dam has no supply water outlet. Supply water is released through

the low level outlet pipe into the stream on an as-needed basis and is diverted into the water distribution system downstream from the dam.

1.3 PERTINENT DATA

Elevations referred to in this section and subsequent sections of the report were obtained from design drawings.

<u>a.</u>	Drainage Area (sq. mi.)	8.0
<u>b.</u>	Discharge at Dam Site (cfs)	
	Spillway at top of flanking earth embankments	4000
	Spillway at top of dam	8820(1)
	Total spillway capacity at top of dam	8820(1)
с.	Elevation (USGS Datum) (feet)	
	Top of dam	1454.9
	Top of earth embankments flanking spillway	1452.5
	Spillway crest	1447.0
	Reservoir drain, invert elevation	1403.0
	Reservoir didin, invert elevation	1403.0
d.	Reservoir (acres)	
	Surface area at top of dam	74.6
	Surface area at crest of spillway	45.4
e.	Storage Capacity (acre-feet)	
	Top of dam	954.0
	Spillway crest	495.0
	bpiliway cicoc	473.0
f.	Dam	
	Туре	Earth embankment
	Length	470 <u>+</u> feet
	Height	54 feet
	Top width	l6 feet
	Side slopes	Downstream: 2H:1V
	•	Upstream: 2.2H:1V
	Zoning	No
	Impervious core	Yes
	Cutoff	Yes
	Grout curtain	No.
		110
g.	Spillway	
	Type	Overflow concrete
		ogee section
	Length	100 feet
	Crest elevation	1447.0
		

⁽¹⁾ Including flow over the earth embankments flanking the spillway.

h. Earth Embankments Flanking Spillway

(Emergency Spillway)

The dam has no formal emergency spillway. However, earth embankments flanking the concrete overflow section are about 2.5 feet below the dam crest level and could function as an emergency spillway. Further description of the embankments are included in Section 1.2 a.

i. Reservoir Drain

Type

Length Access Regulating facility 12-inch and 18-inchdiameter cast iron pipes 250 ± feet Through valve chamber Valves

SECTION 2: ENGINEERING DATA

2.1 DATA AVAILABLE

Available information was obtained from the New York State Department of Environmental Conservation, Dam Safety Division files and from personnel of the Water and Sewer Department, Dansville, New York. Available information includes design drawings dated 1929 and 1933, and a dam inspection report dated 1954.

2.2 GEOLOGY

The Dansville Reservoir Dam is located in the glaciated Allegheny Plateau section of the Appalachian Plateau Province. This region is characterized as a maturely dissected plateau with the topographic features modified by continental glaciation. The modification consists of rounding off of the high areas and deposition of glacial till in the valleys.

The dam site is located just north of a northeast trending anticline (trending approximately north 70 degrees east). The folding is gentle with a maximum dip of the limbs of one to two degrees. The dip of the strata is affected locally by the folding; however, regionally, the rock strata dip south to southwest at approximately 100 to 150 feet per mile. The most prominent fracture orientations in the region have a strike of north 20 to 30 degrees west.

The rock strata in the area consist of unconsolidated Pleistocene glacial till (Wisconsin Drift) underlain by strata of the West Falls Group (Upper Devonian Age). The glacial till consists of a mixture of clay and silt with varying quantities of gravel. The glacial till is relatively thin on hilltops and slopes and thicker in the valleys. The bedrock consists of a thick sequence of interbedded gray to greenish-gray shale, gray silty shale and siltstone, gray calcareous siltstone, gray mudstone, and black fissile shale.

The abutment slopes are relatively gentle and not susceptible to landslide slope movement.

2.3 SUBSURFACE INVESTIGATION

Available information indicates that three test pits, ranging in depth from 9 to 11 feet, were excavated in order to investigate subsurface conditions. The test pit materials were classified as firm clay.

2.4 EMBANKMENT AND APPURTENANT STRUCTURES

Plate 2 shows a plan view of the dam and spillway. Plate 3 shows a detailed plan, section, and details of the dam and appurtenant structures. The dam is a homogeneous embankment with a central

reinforced concrete core wall. A steel sheetpile cutoff wall, having a depth of about 10 feet, is provided across the valley below the concrete core wall. A steel sheetpile cutoff wall was also provided across the spillway ogee section.

The dam has a measured slope of about 2.2 horizontal to 1 vertical on the upstream face and a measured slope of about 2 horizontal to 1 vertical on the downstream face.

The low level outlet facilities include two cast iron pipes (12-inch and 18-inch-diameters). Flow through the pipes is controlled by valves located in a valve chamber at the midpoint of the pipes. As shown in Plate 3, the pipes are supported by a reinforced concrete cradle. Upstream from the valve chamber, the pipes are equipped with concrete cutoff collars.

No reference was found to indicate whether a hydrologic/hydraulic analysis was conducted to size the spillway or outlet structures.

2.5 CONSTRUCTION RECORDS

No construction records are available. Based on visual observations, the dam and the spillway structures appear to be in general conformance with the 1933 design drawing.

2.6 OPERATING RECORDS

None available.

2.7 EVALUATION OF DATA

The information obtained from the state files is considered to be adequate for Phase I inspection purposes.

SECTION 3: VISUAL INSPECTION

3.1 FINDINGS

a. General

Visual inspections of the dam were conducted on June 26 and July 15, 1981. On both dates, the pool level was approximately two feet below the crest level of the spillway.

b. Embankment

No signs of distress, misalignment, or seepage were observed. The faces and crest of the dam are covered with large trees and brush. Most of the larger trees are located on the upstream slope. Growth on the dam is not considered to be extensive enough to significantly hamper inspection. The top of the dam was surveyed relative to the spillway crest level and found to be in the range of 0.1 foot below to 0.4 foot above the design elevation.

c. Primary Spillway

The spillway structure consists of a concrete ogee section located approximately 2,400 feet northwest of the dam. The ogee section is connected to a concrete apron which directs discharge into the natural stream bed downstream from the apron. The concrete at the junction of the ogee section and the apron slabs is deteriorated and undermined. This area is in need of repairs.

d. Emergency Spillway

The dam has no formal emergency spillway. However, earth embankments flanking the concrete overflow section of the primary spillway are about 2.5 feet below the dam crest elevation and could function as an emergency spillway. The flanking embankments are approximately eight feet high adjacent to the concrete spillway overflow section, then gradually merge into the abutments. A further description of the flanking embankments is included in Section 1.2 a. Presently, the embankments are covered with grass, brush and small trees. Visual observations suggest that the embankments may withstand overtopping of up to about one foot without significant erosion. With continued or greater overtopping, partial or complete erosion of the embankments is considered to be likely.

e. Reservoir Drain

The reservoir drain facilities consist of a 12-inch-diameter and an 18-inch-diameter cast iron pipe which extend from the upstream embankment toe to the downstream toe. Flow through these pipes is controlled by manually operated valves located in a valve chamber which extends to the crest of the dam near the center of the dam. The system is reported to be operational, but its operation was not observed.

f. Downstream Channel

The downstream channel below the spillway discharge structure is the natural stream bed. The channel appears to be stable within the vicinity of the spillway. The downstream channel below the reservoir drain facilities is the natural stream bed. The channel appears to be stable within the vicinity of the dam.

g. Reservoir

There are no visible signs of instability or sedimentation problems within the reservoir area.

3.2 EVALUATION

The dam was found to be in fair condition. Large trees on the crest and faces of the dam should be removed. Deteriorating concrete portions of the spillway structure should be repaired.

SECTION 4: OPERATION AND MAINTENANCE PROCEDURES

4.1 PROCEDURES

The reservoir level is normally maintained below the spillway crest elevation by periodically discharging flow through the low level outlet pipes. According to the operating personnel, the intent of this operating procedure is to avoid discharge over the spillway which reportedly causes erosion of the farmland located downstream from the spillway discharge channel.

4.2 MAINTENANCE OF THE DAM

The dam is overgrown with large trees and brush. It does not appear that any attempts have been made to maintain the dam.

4.3 WARNING SYSTEM IN EFFECT

No formal warning system exists for the dam.

4.4 EVALUATION

The maintenance condition of the dam is considered to be poor. As noted before, the dam and spillway are in need of repair and restoration.

SECTION 5: HYDRAULIC/HYDROLOGY

5.1 DRAINAGE AREA CHARACTERISTICS

The Dansville Reservoir Dam drains a watershed of 8.0 square miles. The basin is comprised of woodlands. Relief ranges from gentle to moderate.

5.2 ANALYSIS CRITERIA

As previously stated, Dansville Reservoir Dam is classified as an intermediate dam in the high hazard category. According to the recommended criteria for evaluating spillway discharge capacity, such impoundments are required to pass the full PMF.

The PMF inflow hydrograph for the reservoir was determined using the Dam Safety Version of the HEC-1 computer program developed by the Hydrologic Engineering Center of the U.S. Army Corps of Engineers. The data used for the computer input are presented in Appendix D.

5.3 SPILLWAY CAPACITY

The spillway of the dam consists of a 100-foot-long concrete ogee section. Because the earth embankments on each side of the spillway are below the dam crest level, flow over these sections provides additional spillway capacity. Based on the available head relative to the top of the dam, the combined capacity of the ogee section and low embankments adjacent to the spillway is calculated to be 8820 cfs. The discharge capacity of the 5.5-foot-deep, 100-foot-wide concrete overflow section is calculated to be about 4000 cfs.

5.4 RESERVOIR CAPACITY

The storage capacity of the dam at normal pool level (El. 1447.0) is 495 acre-feet and at the top of dam (El. 1454.9), the storage capacity is 954 acre-feet.

5.5 FLOODS OF RECORD

No data available.

5.6 OVERTOPPING POTENTIAL

The PMF inflow hydrograph, determined according to the recommended procedure, was found to have a peak flow of 12,950 cfs. Various percentages of the PMF inflow hydrograph were routed through the reservoir and it was found that by considering the combined capacity of the ogee overflow section and the adjacent embankment

overflow sections, the dam can pass approximately 70 percent of the PMF without overtopping the dam. Based on the capacity of the ogee section alone, the dam can pass approximately 30 percent of the PMF (reservoir surface at about the crest level of the earth embankment flanking the spillway). Under the full PMF, low areas near the right abutment of the dam will be overtopped for a duration of approximately five hours with a maximum depth of about one foot.

As previously noted, earth embankments flanking the concrete overflow sections of the primary spillway are about 2.5 feet below the dam crest elevation. Therefore, these embankments would be overtopped prior to overtopping of the main dam. Visual observations suggest that erosion of these embankments might begin when overtopped by about one foot; and in that event, these embankments may function as a spillway fuse plug. The discharge capacity of the section will increase with continued erosion of the earth embankments. Because the height of the flanking embankments are approximately equal to the depth of the spillway, flow resulting from continued or full erosion of these sections would be approximately equal to flow from an equivalent width spillway.

5.7 EVALUATION

The spillway was found to pass approximately 70 percent of the PMF without overtopping the dam considering the combined capacity of the spillway and the flow over the embankments flanking the spillway. Because the spillway capacity is less than the required spillway design flood of full PMF, the spillway capacity is rated to be inadequate. As discussed above, the earth embankments flanking the spillway may function as spillway fuse plugs when overtopped, thereby increasing the spillway capacity of the dam.

SECTION 6: STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

a. Visual Observations

As discussed in Section 3, the field observations did not reveal any signs of distress that would significantly affect the stability of the dam at this time and none were reported in the past.

b. Design and Construction Data

Available information, other than the design drawings, included no quantitative data which could aid in the assessment of structural stability of the dam. Based on visual observations, the static stability of the dam is considered to be adequate.

c. Postconstruction Changes

None reported.

d. Seismic Stability

The dam is located in Seismic Zone 2. In this zone, a horizontal acceleration of 0.05g is typically used for preliminary analysis. No data is available relative to the character of the embankment material. Therefore, the adequacy of seismic stability of the embankment could not be assessed.

SECTION 7: ASSESSMENT/RECOMMENDATIONS

7.1 ASSESSMENT

a. Safety

Visual observations indicate that Dansville Reservoir Dam is in fair condition. At this time, no conditions were noted that would seriously affect the overall adequate performance of the dam. Clearing of trees from the faces of the dam and repairs to the spillway concrete are required.

The spillway capacity was evaluated according to the recommended procedure, and the spillway was found to pass approximately 70 percent of the PMF without overtopping the dam. Because the dam cannot pass the recommended spillway design flood of full PMF without overtopping, the spillway is classified to be inadequate. However, it is not considered to be seriously inadequate, because the spillway capacity is greater than 50 percent of the PMF.

b. Adequacy Information

Available information, in conjunction with visual observations, is considered to be sufficient to make a Phase I evaluation.

c. Need for Additional Investigation
No additional investigation is required.

d. Urgency

The following recommendations should be implemented within 12 months from notification to the owner.

7.2 RECOMMENDATIONS

- The trees on the upstream and downstream faces of the dam should be removed under the supervision of a professional engineer. Trees and brush on the earth embankments flanking the concrete overflow section of the spillway should also be cleared.
- 2. The spillway structures should be repaired.
- 3. An emergency action plan should be developed, including a formal warning system to alert the downstream residents in the event of emergencies.
- 4. The dam and appurtenant structures should be inspected regularly and necessary maintenance should be performed.

APPENDIX A

PHOTOGRAPHS



PHOTOGRAPH NO. 1
Dam Crest (looking southwest)



PHOTOGRAPH NO. 2 Upstream Face



PHOTOGRAPH No. 3
Spillway
(Flanking embankment in background in line with spillway crest)



PHOTOGRAPH NO. 4 Voids Under Spillway Slab



PHOTOGRAPH NO. 5
Outlet Works Gatehouse



PHOTOGRAPH NO. 6
Outlet Pipes
(pipe adjacent to smaller outlet pipe is gate chamber drainpipe)



PHOTOGRAPH NO. 7 Railroad Underpass (approximately 1.0 mile downstream)



PHOTOGRAPH NO. 8
Stream Through Dansville
(3.0 miles downstream)

APPENDIX B

VISUAL INSPECTION CHECKLIST

APPENDIX B VISUAL INSPECTION CHECKLIST

1)	Basic	Data

a. General

	Name of Dam Dansville Reservoir Dam					
	Fed. I.D. # N.Y. 431 DEC Dam No. 42-999					
	River Basin Genesee River Basin					
	Location: Town Dansville County Steuben					
	Stream Name Little Mill Creek					
	Tributary of Mill Creek					
	Latitude (N) 42° 34.1' Longitude (W) 77° 38.5'					
	Type of DamEarth					
	Hazard Category High hazard					
	Date(s) of InspectionJune 26, 1981 and July 15, 1981					
	Weather Conditions Cloudy, Warm, Temp. 75 Degrees					
	Reservoir Level at Time of Inspection El. 1445.0					
Ъ.	Inspection Personnel Lawrence Andersen, P.E.; James Poellot,					
	P.E.; Bilgin Erel, P.E.; and Michael Bort					
c.	Persons Contacted (Including Address & Phone No.)					
	Mr. Keith Petti, Superintendent of Water and Sewers,					
	14 Clara Barton Street, Town Hall, Dansville, NY 14437,					
	(716) 335-5270					

	d.	Histo	ry:
		Date	Constructed Unknown Date(s) Reconstructed N/A
		Desi	gner Frank H. Macy, Consulting Engineers, Rochester, NY
		Cons	tructed byUnknown
		Owne	r Village of Dansville, New York
2)	Emb	ankme	nt_
	a.	Char	acteristics
		(1)	Embankment Material Earth
		(2)	Cutoff Type Steel sheetpiles
		(3)	Impervious CoreConcrete core
		(4)	Internal Drainage System None
		(5)	Miscellaneous
	b.	Cres	
		(1)	Vertical Alignment Good (Within 0.4 foot of design
			elevation).
		(2)	Horizontal Alignment Good
		(=)	MOTIZOREAL MIRAMENE
		(2)	
		(3)	Surface Cracks None
		(4)	Miscellaneous
	с.	Upst	ream Slope
		(1)	Slope (Estimate) 2.2H:1V (as measured)
		(2)	Undesirable Growth or Debris, Animal Burrows Covered with
			brush and large trees.
		(3)	Claushing Cubaidance or Depressions Name

(4)	Slope Protection Riprap
(5)	Surface Cracks or Movement at Toe Not visible.
Down	stream Slope
(1)	Slope (Estimate) 2H: IV (as measured)
(2)	Undesirable Growth or Debris, Animal Burrows Covered
	with brush and large trees.
(3)	Sloughing, Subsidence or Depressions None observed.
(4)	Surface Cracks or Movement at Toe None observed.
(5)	Seepage None observed.
	·
(6)	External Drainage System (Ditches, Trenches, Blanket)
	None
(7)	Condition Around Outlet Structure Good
(8)	Seepage Beyond Toe None observed.
Abutı	nents - Embankment Contact
	Good

		(1)	Erosion	at Con	tact	None		
		(2)	Seepage	Along	Contact	None	observed.	
3)	Dra	inage	System					
	а.	Desci	ription o	of Syst	em	None		
	ь.							
				•				
	c.	Disch	narge fro	om Drai	nage Sy	stem	-	
4)	Ins	trumer	ntation (Monume	ntation	/Surveys,	Observation Wells, T	Weirs,
	I LC.	Zomete	:13, E.C.					
								
								
								
			 ,					
								
							· · · · · · · · · · · · · · · · · · ·	

Res	pervoir
a.	SlopesGentle slopes, no problems observed.
b.	Sedimentation Unknown
c.	Unusual Conditions Which Affect Dam None observed.
Are	a Downstream of Dam
a.	Downstream Hazard (No. of Homes, Highways, etc.) A large rail
	road embankment and a New York State Route 63 bridge located
	1.2 and 2.6 miles downstream from the dam, respectively,
	approximately 6 residences located 2.7 miles downstream,
	and the Village of Dansville located 3 miles downstream.
ъ.	Seepage, Unusual Growth None
с.	Evidence of Movement Beyond Toe of Dam None
d.	Condition of Downstream Channel No problem in the vicinity
	of the dam.
Spi	llway(s) (Including Discharge Conveyance Channel)
а.	General Service Spillway: Concrete ogee section located
	approximately 2,400 feet northwest of dam.
	Auxiliary Spillway: No formal emergency spillway.
	However, earth embankments on either side of the
	spillway may function as an emergency spillway.
b.	Condition of Service Spillway Generally satisfactory.
	Deteriorating concrete at the junction of the overflow
	section and the downstream apron slabs.

	c.	Condition of Auxiliary Spillway No formal auxiliary spillway.
		Earth embankments adjacent to the ogee overflow section are
		overgrown with vegetation and small brush.
	d.	Condition of Discharge Conveyance Channel Earth channel,
	u.	
		small trees and brush.
8)	Res	ervoir Drain/Outlet
		Type: Pipe X Conduit Other
		Material: Concrete Metal Other Cast iron
		pipe, Class B
		Size: 12- and 18-inch-diameter Length 250 + feet
		Invert Elevations: Entrance El. 1403 Exit El. 1402.0
		Physical Condition (Describe): Not observable.
		Material:
		Joints: Alignment
		Structural Integrity:
		Hydraulic Capability:
		Means of Control: Gate Valve X Uncontrolled
		Operation: Operable X Inoperable Other
		Present Condition (Describe): The reservoir drainpipes
		are reported to be operable. (Operation not observed.)

Str	uctural
a.	Concrete Surfaces The spillway concrete is generally in
	fair condition except for deterioration and undermining
	at the junction of the ogee section and the discharge
	apron.
ь.	Structural Cracking See note above.
c.	Movement - Horizontal & Vertical Alignment (Settlement)
	None observed.
d.	Junctions with Abutments or Embankments No problems observed.
	·
e.	Drains - Foundation, Joint, Face N/A
f.	Water Passages, Conduits, Sluices N/A
g.	Seepage or Leakage None observed.
	<u> </u>

Joints - Construction, et	tc. N/A
Foundation Unobservab	ble
Abutments N/A	
Control Gates <u>Condit</u>	tion unknown.
Approach & Outlet Channel	ls <u>Good</u>
Energy Dissipators (Plung	ge Pool, etc.) <u>Good</u>
Intake Structures N/A	
Stability N/A	
Miscellaneous	

l0) <u>Ap</u>	ourtenant	Structu	res (Power	House,	Lock,	Gatehouse,	Other)
a.	Descript	ion and	Condition		None		
							
		•					
							
						·	
		,					
			~~~~~~~~~~				
							
							

APPENDIX C

ENGINEERING DATA CHECKLIST

APPENDIX C ENGINEERING DATA CHECKLIST NAME OF DAM: DANSVILLE RESERVOIR DAM

AREA-CAPACITY DATA:

		Elevation (feet)	Surface Area (acres)	Storage Capacity (acre-feet)
1)	Top of Dam (Measured Low Spot)	1454.9	74.6	954.0
2)	Design High Water (Max. Design Pool)	N/A	N/A	N/A
3)	Auxiliary Spillway Crest	N/A	N/A	N/A
4)	Service Spillway Crest	1447.0	45.4	495.0
5)	Crest of Orifice (Normal Pool)	N/A	N/A	N/A

DISCHARGES

		Discharge (cfs)
1)	Average Daily	16 ±
2)	Principal Spillway at Top of Dam(1)	8820
3)	Auxiliary Spillway	N/A
4)	Total (of all facilities) at Maximum High Water	Unknown
5)	Maximum Known Flood	Unknown
6)	At Time of Inspection	<u>1 +</u>

 $⁽¹⁾_{\mbox{Flow}}$ over ogee section and flanking earth embankments.

PAGE C1 OF 4

DAM: <u>Dansville Reser</u>	voir Dam	
CREST ELEVATION: 1454	.9	
Type:Earth		
Width: 16 feet	Length: _	470 <u>+</u> feet
Spillover: 100-foot-wide	concrete ogee secti	on.
Location: Approximately	2,400 feet northwes	t of dam.
SPILLWAY:		
SERVICE		AUXILIARY
		The dam has no formal auxiliary spillway.
1447.0	Elevation	
Ogee section	Type	
100 feet	Width	
	Type of Contro	<u>1</u>
Uncontrolled	Uncontrolled	
	Controlled	
N/A	_ Type (Flashboards; Ga	
N/A	Number	ce/
150 ⁺ feet	Size/Length	
		1
Concrete	Invert Materia	
Unknown	Anticipated Leng of Operating Serv	
N/A	Chute Lengt	h
	eight Between Spills and Approach Channe	

nydrometero	logical dages:
Type:	None
Location	: N/A
Records:	
Date	~ _ N/A
Max.	Reading - N/A
FLOODWATER	CONTROL SYSTEM:
Warning :	System: None
Method o	f Controlled Releases (Mechanisms):
	None

RAINAGE AREA: 8.0 square miles
RAINAGE BASIN RUNOFF CHARACTERISTICS:
Land Use - Type: Woodlands
Terrain - Relief: Gentle to moderate
Surface - Soil: Glacial till (low permeability).
Runoff Potential (existing or planned extensive alterations to existing surface or subsurface conditions)
Moderate runoff potential due to general gentle to
moderate slopes and low infiltration rate.
Potential Sedimentation Problem Areas (natural or man-made; present or future)
None observed.
Potential Backwater Problem Areas for Levels at Maximum Storage Capacity Including Surcharge Storage:
None observed.
Dikes - Floodwalls (overflow and nonoverflow) - Low Reaches Along the Reservoir Perimeter:
Location: None
Elevation:
Reservoir:
Length at Maximum Pool: 2,700+ feet
Length of Shoreline at Spillway Crest: 7,200+ feet

APPENDIX D
HYDROLOGY AND HYDRAULIC ANALYSES

HYDROLOGY AND HYDRAULIC ANALYSIS DATA BASE

NAME OF DAM: Dansville Reservoir Dam (NY DEC 42-999)

PROBABLE MAXIMUM PRECIPITATION (PMP) = 22.0 INCHES/24 HOURS⁽¹⁾

STATION	1	2	3	4	5
Station Description	Dansville Reservoir	Dansville Reservoir Dam.			
Drainage Area (square miles)	8.0	-			
Cumulative Drainage Area (square miles)	8.0	8.0			
Adjustment of PMF for Drainage Area (%)					
6 Hours	116	-		J	}
12 Hours	126	- 1		1	ļ
24 Hours	141	-		ļ	
48 Hours	151	- 1		1	
72 Hours	-	- 1			
Snyder Hydrograph Parameters					
c _p /c _t (2)	0.60/1.87	1 - 1		1	
L (miles)(3)	5.76	- {		ĺ	Į
Lca (miles)(3)	2.65	-		Ì	} .
$t_p = C_t(L \cdot L_{ca})^{0.3}$ (hours)	4.24	-			
Spillway Data	 	+		 	
Crest Length (ft)	-	100.0		1	}
Freeboard (ft)		-		}	}
Discharge Coefficient	_	3.1		}	}
Exponent		1.5		1	l

^{(1) &}lt;u>Hydrometeorological Report 33</u> (Figure 1), U.S. Army, Corps of Engineers, 1956. (2) Snyder's Coefficients.

⁽³⁾ L = Length of longest water course from outlet to basin divide.

Lca = Length of water course from outlet to point opposite the centroid of drainage area.

SNYDER UNIT HYDROGRAPH, SPILLMAY AND DAM OVERTOPPING ANALYSES
UANSVILLE RES. DAM, (NY 42-999).STEUBEN CUUNTY.N.Y. PROJECT NO. HF-774-12
FOR 20x,30x,40x,50x,6cx,7tx,80x,90x,and 10cx probable maximum flocoteme)
0 0 0 0 0 -4 SNYDER INFLOW HYDROGRAPH TO DANSVILLE RES. DAM. (N.Y. 42-995) ROUTING FLOW THROUGH DANSVILLE RESERVOIR DAM, (N.Y. 42-999) 0.76 54.5 1440.0 1450.0 151 09.0 24.0 0.50 16.1 1.5 610.0 580.0 1420.0 3.10 0.40 8.0 2.0 1410.0 100.0 2.65 200.0 0.30 0.00 -0.05 CALC. OF FLOOD MYDNOGRAPH PACKAGE (HEC-1) AM SAFETY VERSION JULY 1978 LAST MODIFICATION UT APR BO ************************* 02.7 \$£1405.0 DAN SAFETY VERSION

1.00

0.96

0.60

0.05

0.1

158.9 *

95.5

610.0

\$60.0

181447.0 \$01454.9

-1447.0

*Reservoir is planimetered from design drawings and USGS topographic maps.

COMPUTER INPUT OVERTOPPING ANALYSIS PAGE D2 OF 4

PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIFLE PLAN-HATIO ECONOMIC COMPUTATIONS FLOWS IN CUBIC FEET PER SECOND (CLBIC METERS PER SECOND) AREA IN SQUARE MILES (SQUARE KILOMETERS)

OPERATION		ST & 1 10M	AREA	PLAN KA	KATIQ 1	RATIG . 2	RATIOS APP RATIO 3	RATIOS APPLIED TO FLOWS ATIQ 1 RATIO 2 RATIO 3 RATIO 4 RATIO 5 HATIO 6 RATIO 7 RATIO H HATIO 9 -20 -30 -40 -50 -60 -70 -80 -40 1.00	0MS RAT10 5	4 411U 6	84116 ?	RATIO H	KATIU 9 1.09
HYDROGRAPH AT	14	_ ~	8.00	-~	2594.	3890. 110.1616	5187.	6484.	7781. 226.3334	9078° 257°0516	293.7736	116/10	12968. 367.211
ROUTED TO		~~	8.00	_ ~	2502.	3776.	5160.	6396.	218.0736	9005.	10348.	11655. 529.9810	12954.

FLOOD ROUTING ANALYSIS PAGE D3 OF 4

SUMMARY OF DAM SAFETY ANALYSIS

PL AN

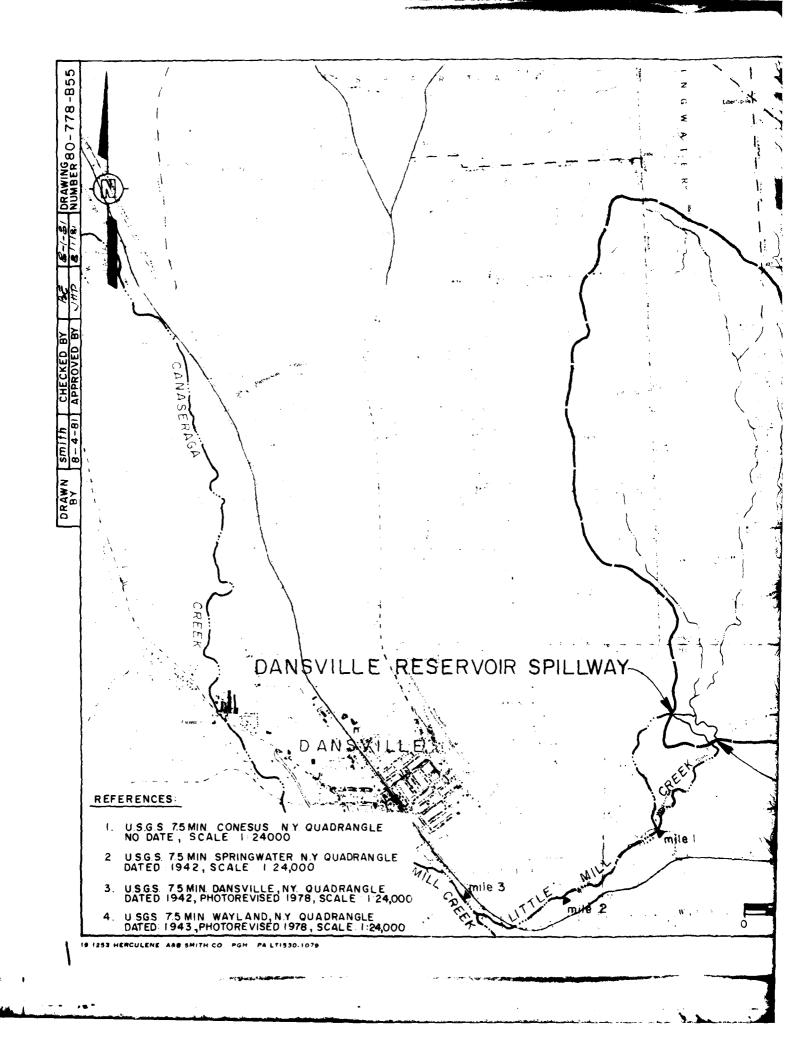
	OF TIME OF TFLOW FAILURE RS HOURS									00 00
1454.911 1454.911 954. 88211.	TIME OF MAX OLTFLUE HOURS	7.44	* 77	7,4)* **	44	44.	44.	7. 44	44.
	DURATION CVER TOP Hours	0.00	<u>ن</u> ، 0	00.00	0,00	0.00	1.10	3.00	6. (id	5.00
SPILLWAY CREST 1447.FU 495. 6.	PAXIMUM OUTFLOW CFS	2502.	3770.	5160.	6396.	7701.	90.03	16348.	11653.	12954.
INITIAL VALUE 1447.00 495.	MAXIMUM Storage AC-FT									1035.
144 144	HAMINUM DEPTH OVER DAM	0.00	00.00	00.0	00.0	07.0	20.	94.	.77	1.04
ELEVATION Storage Outflow	MAXIMUM RESERVOIR W.S.ELEV	1451.02	1452.29*	1453.22	1453.88	1454.45	1454.97	1455.36	1455.67	1455.94
	RATIO OF PMF	•20	.30	07.	.50	99.	2.0	08.	06.	1.00

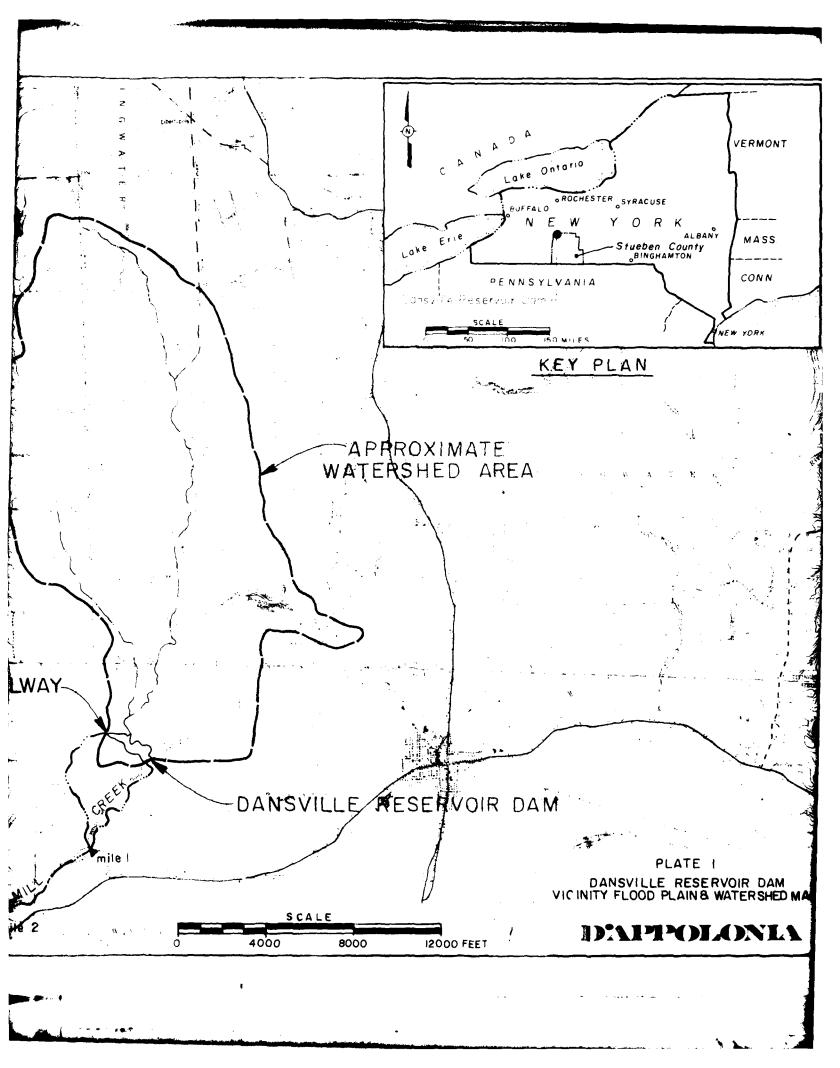
*The top of the earth embankments flanking the spillway is at Elevation 1452.5.

OVERTOPPING ANALYSIS SUMMARY PAGE D4 OF 4

APPENDIX E

PLATES





NG 80 - 778-B56 Kidd Zimmer Fronk Her 19 1253 MERCULENE. ABS SMITH CO . PGH . PA LT1530-1079

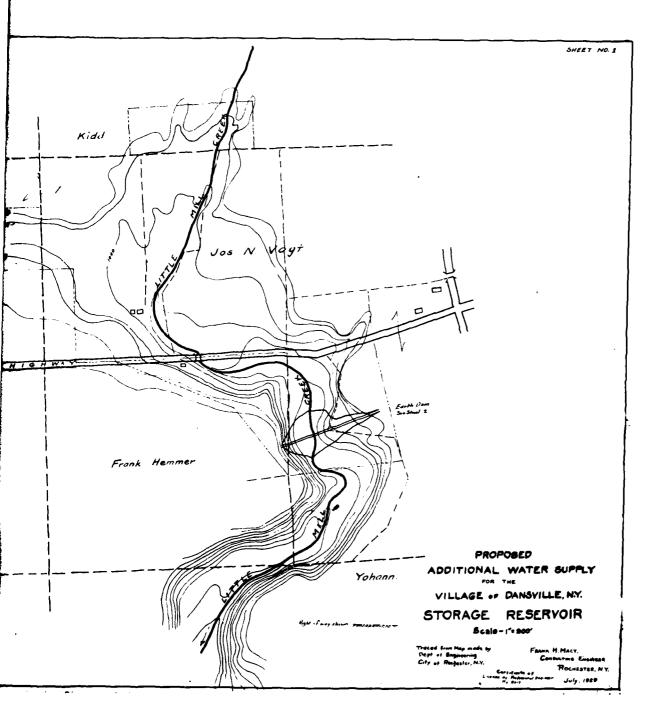
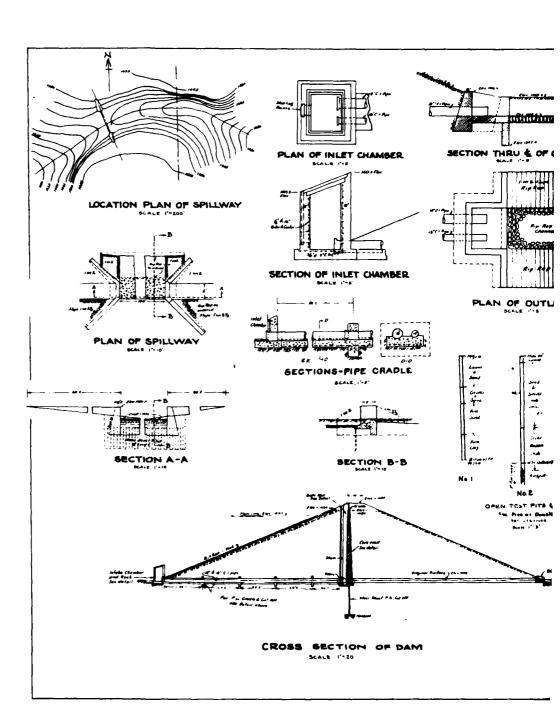


PLATE 2

DAPPOLONIA



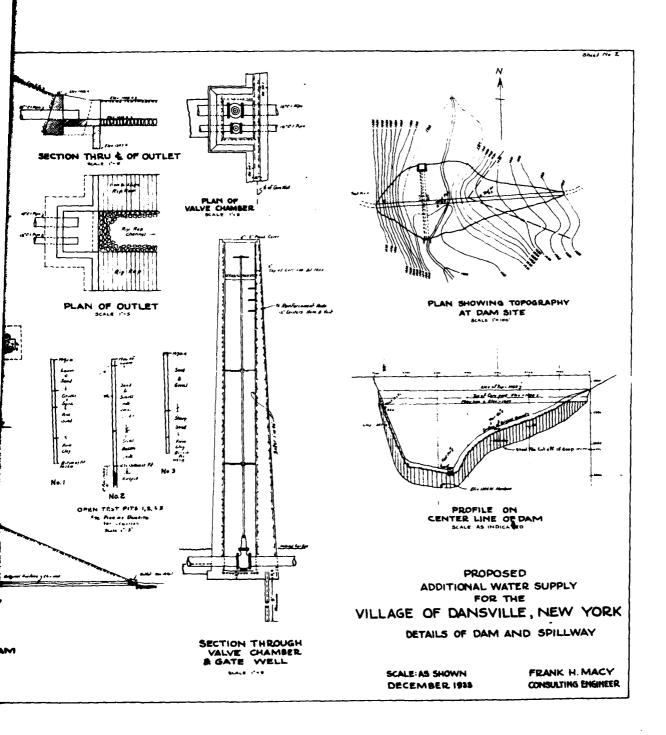
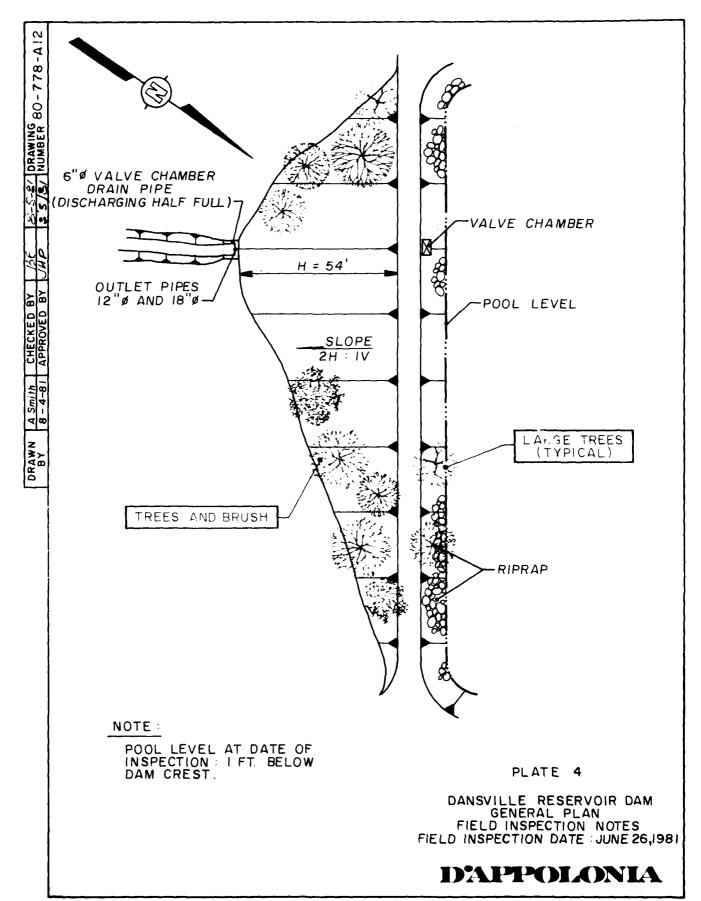


PLATE 3

DAPPOLONIA



APPENDIX F

GEOLOGY MAP

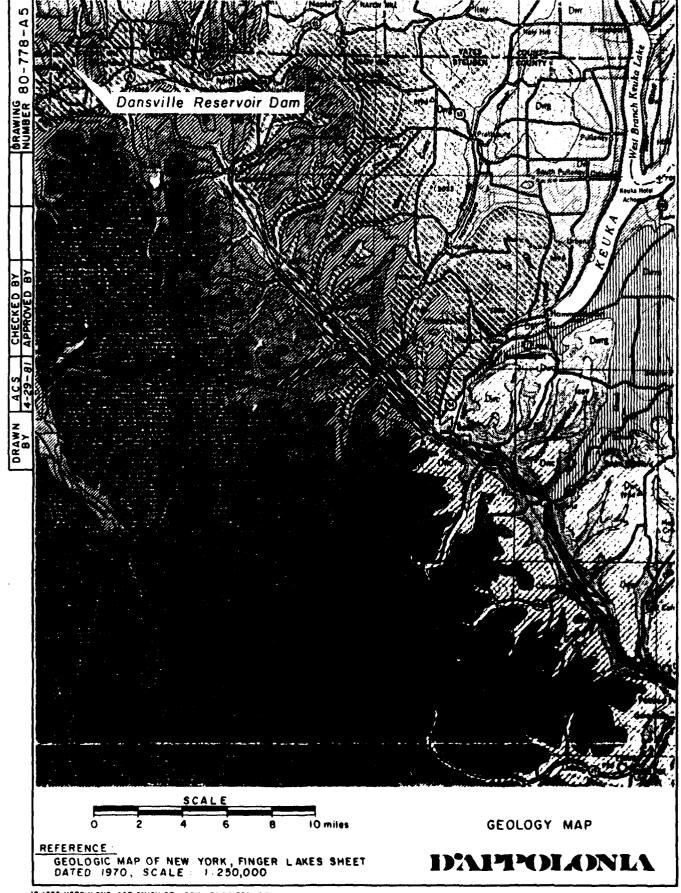
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nga.

.

.

V.X.



LEGEND

 D_{i}

Dw

Ds

CANADAWAY GROUP 800-1200 ft. (240-370 m.)



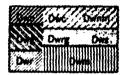
Machias Formation—shale, siltstone; Rushford Sandstone; Caneadea, Canisteo, and Hume Shales; Canaseraga Sandstone; South Wales and Dunkirk Shales; In Pennsylvania: Towanda Formation—shale, sandstone.

JAVA GROUP 300-700 ft. (90-210 m.)



Wiscoy Formation—sandstone, shale; Hanover and Pipe Creek Shales.

WEST FALLS GROUP 1100-1600 ft. (340-490 m.)



Dwn
Dwg
West Hill and Gardeau Formations—shale, siltstone;
Roricks Glen Shale; upper Beers Hill Shale; Grimes
Siltstone

lower Beers Hill Shale; Dunn Hill, Millport, and Moreland Shales.

Ow: Nunda Formation—sandstone, shale; West Hill Formation—shale, siltstone; Corning Shale.

Owner "New Milford" Formation—sandstone, shale.

Dwis Gardeau Formation—shale, siltstone; Roricks Glen

Shale
Own Slide Mountain Formation—sandstone, shale, conglomerate.

Dwar Beers Hill Shale: Grimes Siltstone; Dunn Hill, Millport, and Moreland Shales

SONYEA GROUP 200-1000 ft. (60-300 m.)



in west: Cashagua and Middlesex Shales. In east: Rye Point Shale; Rock Stream ("Enfield") Siltstone; Pulteney, Sawmill Creek, Johns Creek, and Montour Shales.

GENESEE GROUP AND TULLY LIMESTONE 200-1000 ft. (60-300 m.)



Dg West Rive: Shale; Genundewa Limestone; Penn Yan and Geneseo Shales; all except Geneseo replaced eastwardly by Ithaca Formation—shale. siltstone and Sherburne Siltstone.

Ogo Oneonta Formation—shale, sandstone.
Ogo Unadilla Formation—shale, siltstone.
Oi Tully Limestone

LOCKPORT GROUP 80-175 ft. (25-55 m.)



Oak Orchard and Penfield Dolostones, both replaced eastwardly by Sconondoa Formation—limestone, dolostone.

GEOLOGY MAP LEGEND

REFERENCE

GEOLOGIC MAP OF NEW YORK, FINGER LAKES SHEET DATED: 1970, SCALE 1 250,000

D'APPOLONIA

10 1253 HERCULENE. AGG SMITH CO. POH. PA LTISSO-1079

APPENDIX I

REFERENCES

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APPENDIX I

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